



# Control Systems in the Presence of Actuators or Sensors Degradation

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## ABSTRACT

In this paper, we design controller that combines an observer and a control to handle systems subject to actuator or sensor degradation (including complete failure). The observer contains a pre-filter, an adaptive law, and a modified Luenberger observer that achieves estimation of system state and estimation of conditions of actuator or sensor. We have shown that if a set of differential Riccati inequities (DRI) is satisfied then the system can be stabilized under actuator degradation. While in sensor degradation case if an Algebraic Riccati inequality (ARI) and a DRI are satisfied then the system is stabilized.

**Keywords**—*Algebraic Riccati Inequality (ARI); Differential Riccati Inequality (DRI); Linear Matrix Inequality (LMI); Differential Linear Matrix Inequalities (DLMI); Degradation.*

## I. Introduction

Reliable control has been studied with one major assumption that the degradation of actuator or sensor is *a priori*, see for example [2], [4], [5], and [6]. We know that in some system this is not always the case, for example sensor and actuator array systems. In this paper we design an observer-based control system in which the function of observer has been extended not only performs system state estimation but, more importantly, estimates degraded condition of actuator or sensor. It is this idea that builds the observer that has three components: a pre-filter, an adaptive law,

and a modified Luenberger observer. The pre-filter provides a filtered information from sensor output that is used for adaptive law to compute (or monitor) the condition of actuator or sensor. The modified Luenberger observer then gives an estimate of system state. Lastly, a control gain that is computed to compensate the actuator or sensor degradation according to the degraded information of actuator or sensor and system state from observer.

In the case of sensor degradation, the computation of control gain is straightforward once we had the estimation system state from modified Luenberger observer. However, in the presence of actuator degradation the design of control gain must compensate degraded actuator, which complicates the design. We have shown that if a set of DRI is satisfied, then the system can be stabilized in the actuator case. While in sensor case we need to satisfy an ARI and a DRI to stabilize the system. Block diagram in Figure 1 shows structure of the designed system.

Note that we use  $diag(\xi(t))$  to represent a diagonal matrix with its element  $\xi_1, \xi_2, \dots, \xi_m$  and the dimension is determined by its contents, i.e.,

$$diag(\xi(t)) = \begin{bmatrix} \xi_1(t) & 0 & 0 & 0 \\ 0 & \xi_2(t) & 0 & 0 \\ 0 & 0 & \ddots & 0 \\ 0 & 0 & 0 & \xi_m(t) \end{bmatrix}$$

## II. Study of Sensor Degradation

Consider the following system

$$\begin{aligned} \dot{x}(t) &= Ax(t) + Bu(t) \\ y(t) &= Cx(t) \\ y_s(t) &= \text{diag}(\phi(t))y(t) \end{aligned} \tag{1}$$

where the  $x(t) \in R^n$  represents the control input,  $y(t) \in R^v$  is the system output, and  $y_s(t) \in R^v$  is the true signal output of the system from sensors. The diagonal element of  $\text{diag}(\phi(t))$ ,  $\phi_k(t) \in R$ ,  $k = 1, \dots, v$ , is to represent the remaining function of the associated sensor. For example, if an sensor  $\phi_k = 0.80$ , then we say the sensor has 80% functioning.  $u(t) \in R^m$  is the control signals that will be fed into the actuators with observed state ( $\hat{x}(t)$ ) as the feedback signals, i.e.

$$u(t) = K\hat{x}(t) \tag{2}$$

with  $K$  the feedback gain.

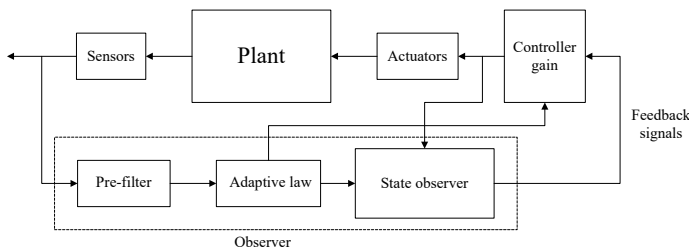


Figure 1 Block diagram of system structure

We now consider a state observer of following form:

$$\begin{aligned} \dot{\hat{x}}(t) &= A\hat{x}(t) + Bu(t) + L(y_s(t) - \text{diag}(\hat{\phi}(t))C\hat{x}(t)) \\ \hat{y}(t) &= C\hat{x}(t) \end{aligned} \tag{3}$$

where  $\hat{x}(t) \in R^n$  is the state of observer,  $L$  is the observer gain to be designed,  $\hat{y}(t) \in R^v$  is an estimation of  $y(t)$  and the true sensor output  $y_s(t)$  is estimated by  $(\text{diag}(\hat{\phi}))\hat{y}(t)$ . The construction of  $\hat{\phi}(t)$  is such that  $\phi(t)$  is estimated.

In here a class of sensor degradation functions will be defined. Consider  $\phi_k(t)$  for all  $k = 1, 2, \dots, v$ . We require  $\phi_k(t)$  satisfy the following properties:

- (1)  $\phi_k(t) \in [0, 1]$ .
- (2)  $\lim_{\Delta t \rightarrow 0} \frac{\Delta\phi_k(t_i)}{\Delta t} = 0$  where  $\Delta\phi_k(t_i) = \phi_k(t_i + \Delta t) - \phi_k(t_i)$ , except at some time instance that  $\phi_k(t)$  jumps toward zero.

The properties addressed above have the following interpretations:

- (1)  $\phi_k(t) = 0$  means the actuator fails.  $\phi_k(t) = 1$  means the actuator works properly. A degraded actuator will be  $0 < \phi_k(t) < 1$ .

$\lim_{\Delta t \rightarrow 0} \frac{\Delta\phi_k(t_i)}{\Delta t} = 0$  means that the degradation is a piecewise constant process. Under the process we allow  $\phi_k(t)$  to have jumps toward zero.

We now state the observer and controller problem for the sensor degradation case as follows.

**Problem 1** Consider the system (1) with controller (2) and observer(3). Find, if possible, the controller and observer which comprises of a pre-filter, an adaptive law for  $\hat{\phi}(t)$ , and a state observer of  $\hat{x}(t)$  with gain  $L$  such that

- (A)  $\hat{\phi}(t)$  is an estimate of  $\phi(t)$  and  $\|\hat{\phi}(t) - \phi(t)\|$  is bounded (which will always be the case if  $0 \leq \hat{\phi}_k(t) \leq 1$  since  $0 \leq \phi_k(t) \leq 1$  for all  $k = 1, \dots, v$ ).
- (B)  $\hat{x}(t)$  converges to  $x(t)$ , i.e.  $\lim_{t \rightarrow \infty} (\hat{x}(t) - x(t)) = 0$ .
- (C) The state observer is asymptotically stable.
- (D) The controller  $u(t) = K\hat{x}(t)$  is such that the closed-loop system with observer achieving (A), (B), and (C) is asymptotically stable.

**Theorem 2** Problem 1 has a solution, if there exist a pre-filter (or error filter)

$$\dot{\tilde{x}} = A\tilde{x} + Ly_s - L(\text{diag}(\hat{\phi}))C\hat{x} \tag{4}$$

an adaptive law

$$\dot{\hat{\phi}}(t) = \begin{cases} \Gamma(\text{diag}(\hat{y}))^T L^T Q\tilde{x} & \forall \hat{\phi}(t) \in D \\ -\Gamma W\hat{\phi}(t) + \Gamma(\text{diag}(\hat{y}))^T L^T Q\tilde{x} & \forall \hat{\phi}(t) \in \bar{D} \end{cases} \tag{5}$$

where

$$D = \left\{ \hat{\phi}(t) \mid \|\hat{\phi}(t)\|^2 \leq \frac{\lambda_v v}{\sigma_v} \right\}, \quad \bar{D} = \left\{ \hat{\phi}(t) \mid \|\hat{\phi}(t)\|^2 > \frac{\lambda_v v}{\sigma_v} \right\}$$

$\lambda_v$  and  $-\sigma_v$  are the maximum eigenvalues of

$$W^T S^{-1} W > 0 \quad \text{and} \quad -W - W^T + S < 0,$$

respectively, for some positive definite symmetric matrices  $W$  and  $S$ .

a state observer

$$\dot{\hat{x}}(t) = A\hat{x}(t) + Bu(t) + L(y_s(t) - \text{diag}(\hat{\phi}(t))C\hat{x}(t)) \quad (6)$$

and a controller

$$u(t) = K\hat{x}(t)$$

such that the following conditions are achieved,

(1) The matrices  $P$  and  $K$  satisfying

$$P = P^T > 0 \quad (7)$$

$$(A + BK)^T P + P(A + BK) < 0$$

(2) The matrices  $Q$ , and  $L$  satisfying

$$Q = Q^T > 0 \quad (8)$$

$$\dot{Q} + (A - L(\text{diag}(\hat{\phi}))C)^T Q + Q(A - L(\text{diag}(\hat{\phi}))C) < 0$$

Proof. See Appendix A for proof.

**Remark 3** From (7) and (8), it is obvious that the computation for  $K$  and  $L$  is independent. The computation for  $K$  is straightforward by transforming to LMI [1], [3]. Likewise by transforming (8) from DRI to differential linear matrix inequalities (DLMI) the solution method developed in [7] can be employed.

### III. Study of Actuator Degradation

Consider the following system

$$\dot{x}(t) = Ax(t) + B(\text{diag}(\xi(t)))u_c(t) \quad (9)$$

$$y(t) = Cx(t)$$

where the  $x(t) \in R^n$  is the state and  $y(t) \in R^v$  is the output of the system.  $\text{diag}(\xi(t))$  with its diagonal element  $\xi_k(t) \in R, k = 1, \dots, m$ , represents the remaining function of the associated actuator.  $u_c(t) \in R^m$  is the computed control signals that will be fed into the actuators with observed state ( $\hat{x}(t)$ ) as the feedback signals, i.e.

$$u_c(t) = K\hat{x}(t) \quad (10)$$

with  $u_c(t) = [u_1^T \ u_2^T \ \dots \ u_m^T]^T$  and  $K$  the feedback gain.

We consider a state observer of following form:

$$\dot{\hat{x}}(t) = A\hat{x}(t) + B\hat{u}(t) + L(y(t) - C\hat{x}(t)) \quad (11)$$

where  $\hat{x}(t)$  is the estimated state,  $L$  is the observer gain to be designed, and  $\hat{u}(t)$  has the form:

$$\hat{u}(t) = (\text{diag}(\hat{\xi}(t)))u_c(t) \quad (12)$$

where the  $\hat{\xi}(t)$  is the estimate of  $\xi(t)$ .

Define the error  $\tilde{x}(t) = \hat{x}(t) - x(t)$  then we have

$$\dot{\tilde{x}} = (A - LC)\tilde{x} + B(\text{diag}(\tilde{\xi}))u_c \quad (13)$$

where  $\text{diag}(\tilde{\xi}(t)) = \text{diag}(\hat{\xi}(t)) - \text{diag}(\xi(t))$

The class of actuator degradation functions is defined in the same similar way as we have defined for sensor degradation function  $\phi(t)$ , which we will not address here. We state the control problem for the actuator degradation as follows.

**Problem 4** Consider the system (9) with controller (10) and state observer (11). Find, if possible, the controller with gain  $K$  and observer which comprises a pre-filter, an adaptive law for  $\hat{\xi}(t)$ , and a state observer of  $\hat{x}(t)$  with gain  $L$  such that

(A)  $\hat{\xi}(t)$  is an estimate of  $\xi(t)$  and  $\|\hat{\xi}(t) - \xi(t)\|$  is

bounded (which will always be the case if  $0 \leq \hat{\xi}_k(t) \leq 1$  since  $0 \leq \xi_k(t) \leq 1$  for all  $k = 1, \dots, m$ ).

(B)  $\hat{x}(t)$  converges to  $x$ , i.e.  $\lim_{t \rightarrow \infty} (\hat{x} - x) = 0$ .

(C) The state observer is asymptotically stable, i.e.  $\sigma(A - LC) \subset C^-$ .

(D) The controller  $u_c(t) = K\hat{x}(t)$  is such that the closed-loop system with observer achieving (A), (B), and (C) is asymptotically stable.

**Theorem 5** Problem 4 has solution if there exist a pre-filter (or  $e_f$  filter)

$$\dot{e}_f(t) = (A - LC)e_f(t) + G(C\hat{x}(t) - y(t)) \quad (14)$$

an adaptive law

$$\dot{\hat{\xi}}(t) = \begin{cases} -\Gamma(\text{diag}(u_c))^T B^T Q e_f & \forall \hat{\xi}(t) \in D \\ -\Gamma W \hat{\xi}(t) - \Gamma(\text{diag}(u_c))^T B^T Q e_f & \forall \hat{\xi}(t) \in \bar{D} \end{cases} \quad (15)$$

where

$$D = \left\{ \hat{\xi}(t) \mid \|\hat{\xi}(t)\|^2 \leq \frac{\lambda_m m}{\sigma_m} \right\},$$

$$\bar{D} = \left\{ \hat{\xi}(t) \mid \|\hat{\xi}(t)\|^2 > \frac{\lambda_m m}{\sigma_m} \right\},$$

$\lambda_m$  and  $-\sigma_m$  are the maximum eigenvalues of  $W^T S^{-1} W > 0$  and  $-W - W^T + S < 0$ , respectively, for some positive definite symmetric matrices  $W$  and  $S$ .  
a state observer

$$\dot{\hat{x}}(t) = A\hat{x}(t) + B(\text{diag}(\hat{\xi}(t))u_c(t) + L(y(t) - C\hat{x}(t))) \quad (16)$$

and a controller

$$u_c(t) = K\hat{x}(t) \quad (17)$$

such that the following conditions are achieved.

(1) The matrices  $P$ ,  $K$  and a scalar  $\gamma > 0$  satisfying

$$P = P^T > 0$$

$$\dot{P} + (A + B(\text{diag}(\hat{\xi}))K)^T P + P(A + B(\text{diag}(\hat{\xi}))K) + \bar{c}K^T K + \frac{\gamma}{b}PBB^T P < 0 \quad (18)$$

for  $\bar{c} > 0$  and  $b > 0$  that are picked by the designer.

(2) The matrices  $Q$ , and  $L$  satisfying

$$Q = Q^T > 0 \quad (19)$$

$$\dot{Q} + (A - LC)^T Q + Q(A - LC) + \gamma(\bar{c}K^T K + F) < 0$$

for a given  $K$ , and

$$F = - \left( \begin{array}{c} PB(\text{diag}(\hat{\xi}))K \\ + \bar{c}K^T K \end{array} \right) \left( \begin{array}{c} (A + B(\text{diag}(\hat{\xi}))K)^T P \\ + P(A + B(\text{diag}(\hat{\xi}))K) \\ + \bar{c}K^T K + \frac{\gamma}{b}PBB^T P \end{array} \right)^{-1} \left( \begin{array}{c} PB(\text{diag}(\hat{\xi}))K \\ + \bar{c}K^T K \end{array} \right)$$

(3) Verify that there exists  $H$  satisfying

$$H = H^T > 0 \quad (20)$$

$$\dot{H} + (A - LC)^T H + H(A - LC) + \frac{1}{a}(H + Q)BB^T(H + Q) < 0$$

given  $Q$ ,  $L$ , and scalar  $a = c - b > 0$  and  $c = \gamma\bar{c}$ .

(4) The matrix  $G$  is such that

$$\left( \begin{array}{c} \dot{Q} + (A - LC)^T Q + Q(A - LC) \\ + \bar{c}(K^T K + F) \end{array} \right) - C^T G^T H$$

$$\left( \begin{array}{c} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{array} \right)^{-1} HGC < 0$$

holds for a pick matrix  $\bar{G}$  and  $G = \rho\bar{G}$ , find  $\rho > 0$  satisfying

$$\rho^2 \alpha - \beta > 0 \quad (21)$$

where

$$\beta = \text{eig}_{\max}[\dot{Q} + (A - LC)^T Q + Q(A - LC) + \gamma(\bar{c}K^T K + F)]$$

$$\alpha = \text{eig}_{\min} \left[ C^T \bar{G}^T H^T \left( \begin{array}{c} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{array} \right)^{-1} H\bar{G}C \right].$$

Note that such the  $\rho$  always exists.

Proof. See Appendix B for proof.

### Remark 6

- (1) It is obvious that the computation of  $L$  in (19) is not independent of (18). However, the computation of (18) can actually be made alone. The technique to solve (18) can be found in [3], which is similar to the solution for (8) in Theorem 2. Once we had the matrices  $P$  and  $K$ , the computation for (19), (20), and (21) may be straightforward by following the similar procedure.
- (2) We note that to deal with actuator degradation is much more complex than the sensor degradation case. This may be due to that in sensor degradation case we receive the degraded information of sensor directly, while in actuator degradation we have only a filtered version of information. Thus to take care of this information discrepancy the pre-filter is designed in such a way that the discrepancy can be asymptotically demolished and thus the system is stabilized. This detail is seen in the proof.

### IV. Conclusion

In this paper, we present an observer-based design to handle actuator or sensor degradation. The observer

contains a pre-filter, an adaptive law, and a modified Luenberger observer that achieves estimation of system state and the estimation of conditions of actuator or sensor. We have shown that if a set of differential Riccati inequities (DRI) is satisfied then the system can be stabilized under actuator degradation. While in sensor degradation case an Algebraic Riccati inequality (ARI) and a DRI must be satisfied to stabilize the system.

**Appendix A**

Proof.

Consider the system (1) with sensor degradation, observer (3), and control signal in (2).

Let error be  $\tilde{x} = \hat{x} - x$ , thus (1) can be rewritten as

$$\dot{\tilde{x}} = (A + BK)x + BK\tilde{x} \tag{A.1}$$

The error  $\tilde{x}(t)$  is given as

$$\begin{aligned} \dot{\tilde{x}} &= A\tilde{x} + L(diag(\hat{\phi}))y - L(diag(\hat{\phi}))C\hat{x} \\ &= (A - L(diag(\hat{\phi}))C)\tilde{x} - L(diag(\tilde{\phi}))Cx \end{aligned} \tag{A.2}$$

where  $diag(\tilde{\phi}) = diag(\hat{\phi}) - diag(\phi)$ .

The usual Lyapunov stability theory cannot be used due to the assumption that the sensor is subject to piecewise constant function. An extension of Lyapunov stability has been proved [3], [8] to guarantee the asymptotic stability of the system. By [8] we need to prove that, by defining a positive definite function, the sum of all increments of the positive definite function for all jump instance is bounded and the derivative of the function is always less than zero (not at jumps). We define a positive definite quadratic function as

$$V = \tilde{x}^T Q \tilde{x} + x^T (\gamma P)x + \tilde{\phi}^T \Gamma^{-1} \tilde{\phi} \tag{A.3}$$

for positive definite symmetric matrices  $Q, P$ , and  $\Gamma$  and a scalar  $\gamma > 0$ .

It can be shown that the total increment of function  $V$  of (A.3) for all jump instance is bounded above, see [3] for detail. The derivative of  $V$  is given

$$\dot{V} = \begin{pmatrix} \dot{\tilde{x}}^T Q \tilde{x} + \tilde{x}^T Q \dot{\tilde{x}} + \tilde{x}^T \dot{Q} \tilde{x} + \dot{x}^T (\gamma P)x \\ + x^T (\gamma P)\dot{x} + x^T (\dot{\gamma P})x \\ + \tilde{\phi}^T \Gamma^{-1} (\dot{\tilde{\phi}} - \dot{\phi}) + (\dot{\tilde{\phi}} - \dot{\phi})^T \Gamma^{-1} \tilde{\phi} \end{pmatrix} \tag{A.4}$$

Substituting (A.1) and (A.2) into (A.4), we have

$$\dot{V} = \begin{pmatrix} \tilde{x}^T \left( \dot{Q} + (A - L(diag(\hat{\phi}))C)^T Q \right) \tilde{x} \\ + x^T (\gamma \dot{P} + \gamma(A + BK)^T P + \gamma P(A + BK))x \\ + x^T \gamma PBK\tilde{x} + \tilde{x}^T \gamma K^T B^T Px \\ - (Cx)^T (diag(\tilde{\phi}))^T L^T Q \tilde{x} - \tilde{x}^T QL(diag(\tilde{\phi}))Cx \\ + \tilde{\phi}^T \Gamma^{-1} (\dot{\tilde{\phi}} - \dot{\phi}) + (\dot{\tilde{\phi}} - \dot{\phi})^T \Gamma^{-1} \tilde{\phi} \end{pmatrix} \tag{A.5}$$

Note that  $diag(\tilde{\phi})Cx = (diag(C\hat{x}))\tilde{\phi}$  and thus (A.5) can be rewritten as

$$\begin{aligned} \dot{V} &= \begin{bmatrix} x \\ \tilde{x} \end{bmatrix}^T \begin{bmatrix} \gamma \dot{P} + \gamma(A + BK)^T P + \gamma P(A + BK) \\ \gamma K^T B^T P \end{bmatrix} \\ &\quad + \begin{bmatrix} \gamma PBK \\ \dot{Q} + A - L(diag(\phi))C \\ + Q(A - L(diag(\phi))C) \end{bmatrix} \begin{bmatrix} x \\ \tilde{x} \end{bmatrix} \\ &\quad - \tilde{\phi}^T (diag(Cx))^T L^T Q \tilde{x} - \tilde{x}^T QL(diag(Cx))\tilde{\phi} \\ &\quad + \tilde{\phi}^T \Gamma^{-1} (\dot{\tilde{\phi}} - \dot{\phi}) + (\dot{\tilde{\phi}} - \dot{\phi})^T \Gamma^{-1} \tilde{\phi} \end{aligned} \tag{A.6}$$

Note that we replace  $-\tilde{\phi}^T (diag(Cx))^T L^T Q \tilde{x}$  by  $-\tilde{\phi}^T (diag(C\hat{x}))^T L^T Q \tilde{x}$  since  $\hat{x}(t) \rightarrow x(t)$  and then  $\tilde{x}(t) \rightarrow 0$ . Therefore, we may have

$$\begin{aligned} \dot{V} &= \begin{bmatrix} x \\ \tilde{x} \end{bmatrix}^T \begin{bmatrix} \gamma(A + BK)^T P + \gamma P(A + BK) \\ \gamma K^T B^T P \end{bmatrix} \\ &\quad + \begin{bmatrix} \gamma PBK \\ (A - L(diag(\phi))C)^T Q \\ + Q(A - L(diag(\phi))C) \end{bmatrix} \begin{bmatrix} x \\ \tilde{x} \end{bmatrix} \\ &\quad - \tilde{\phi}^T (diag(C\hat{x}))^T L^T Q \tilde{x} - \tilde{x}^T QL(diag(C\hat{x}))\tilde{\phi} \\ &\quad + \tilde{\phi}^T \Gamma^{-1} (\dot{\tilde{\phi}} - \dot{\phi}) + (\dot{\tilde{\phi}} - \dot{\phi})^T \Gamma^{-1} \tilde{\phi} \end{aligned} \tag{A.7}$$

To maintain stability we require

$$\begin{bmatrix} \gamma(A + BK)^T P + \gamma P(A + BK) \\ \gamma K^T B^T P \\ \gamma PBK \\ (A - L(diag(\phi))C)^T Q \\ + Q(A - L(diag(\phi))C) \end{bmatrix} < 0 \tag{A.1}$$

and

$$-\tilde{\phi}^T (diag(C\hat{x}))^T L^T Q\tilde{x} - \tilde{x}^T QL(diag(C\hat{x}))\tilde{\phi} + \tilde{\phi}^T \Gamma^{-1}(\dot{\hat{\phi}} - \dot{\phi}) + (\dot{\hat{\phi}} - \dot{\phi})^T \Gamma^{-1}\tilde{\phi} \leq 0 \tag{A.9}$$

It is proved in [3] that (A.1) is equivalent to

$$\begin{cases} (A+BK)^T P + P(A+BK) < 0 \\ (A-L(diag(\hat{\phi}))C)^T Q + Q(A-L(diag(\hat{\phi}))C) < 0 \end{cases} \tag{A.10}$$

[3] proves that (A.9) can also be guaranteed by

$$\dot{\hat{\phi}}(t) = \begin{cases} \Gamma(diag(C\hat{x}))^T L^T Q\tilde{x} & \forall \hat{\phi}(t) \in D \\ -\Gamma W\hat{\phi}(t) + \Gamma(diag(C\hat{x}))^T L^T Q\tilde{x} & \forall \hat{\phi}(t) \in \bar{D} \end{cases} \tag{A.11}$$

where

$$D = \left\{ \hat{\phi}(t) \mid \|\hat{\phi}(t)\|^2 \leq \frac{\lambda_v \nu}{\sigma_v} \right\} \text{ and } \bar{D} = \left\{ \hat{\phi}(t) \mid \|\hat{\phi}(t)\|^2 > \frac{\lambda_v \nu}{\sigma_v} \right\}$$

where the  $\nu$  is number of sensors.  $\lambda_v$  and  $-\sigma_v$  are the maximum eigenvalues of  $W^T S^{-1}W > 0$  and  $-W - W^T + S < 0$ , respectively, for some positive definite symmetric matrices  $W$  and  $S$ .

### Appendix B

#### Proof.

Consider the system (9) with the controller  $u_c(t) = K\hat{x}$  and define error as  $\tilde{x} = \hat{x} - x$ . We have

$$\begin{aligned} \dot{\tilde{x}}(t) &= Ax + B(diag(\xi))u_c \\ &= (A + B(diag(\hat{\xi})))Kx \\ &\quad + B(diag(\hat{\xi}))K\tilde{x} - B(diag(\xi))u_c \end{aligned} \tag{B.1}$$

We construct a pre-filter  $e_f(t)$  and  $G$  satisfying

$$\dot{e}_f = (A - LC)e_f + G(C\hat{x} - y) \tag{B.2}$$

The derivative of  $\tilde{x}$  can be computed

$$\dot{\tilde{x}} = (A - LC)\tilde{x} + B(diag(\tilde{\xi}))u_c \tag{B.3}$$

Define  $\varepsilon = \tilde{x} - e_f$  then

$$\dot{\varepsilon} = \tilde{\dot{x}} - \dot{e}_f = (A - LC)\varepsilon + B(diag(\tilde{\xi}))u_c - GC\tilde{x} \tag{B.4}$$

Note that the construction of  $e_f$  is obvious since  $\tilde{\xi}(t)$  in (B.3) is not known and thus  $e_f$  may be used for approaching  $\tilde{x}(t)$  asymptotically. Now the idea of proof of stability is similar to what we had for the

previous proof in Appendix A. Let positive definite quadratic function be

$$V = x^T (\gamma P)x + \tilde{x}^T Q\tilde{x} + \varepsilon^T H\varepsilon + \tilde{\xi}^T \Gamma^{-1}\tilde{\xi}$$

where  $H$ ,  $Q$ , and  $P$  are positive definite symmetric matrices.  $\gamma \in \mathbb{R}$  and  $\gamma > 0$ . The upper bound of total increments of  $V$  for jump instance is shown in [3].

Thus the derivative of  $V$  is given

$$\dot{V} = \begin{pmatrix} \dot{x}^T (\gamma P)x + x^T (\gamma P)\dot{x} + x^T (\gamma \dot{P})x \\ + \tilde{x}^T Q\dot{\tilde{x}} + \tilde{x}^T Q\dot{\tilde{x}} + \tilde{x}^T \dot{Q}\tilde{x} \\ + \varepsilon^T H\dot{\varepsilon} + \varepsilon^T H\dot{\varepsilon} + \varepsilon^T \dot{H}\varepsilon \\ + \tilde{\xi}^T \Gamma^{-1}(\dot{\tilde{\xi}} - \dot{\xi}) + (\dot{\tilde{\xi}} - \dot{\xi})^T \Gamma^{-1}\tilde{\xi} \end{pmatrix} \tag{B.5}$$

Substituting (B.1), (B.3), and (B.4) into (B.5), we have

$$\dot{V} = \begin{pmatrix} x^T \left[ \gamma \dot{P} + (A + B(diag(\hat{\xi})))K \right]^T (\gamma P) x \\ + (\gamma P)(A + B(diag(\hat{\xi})))K \\ + \tilde{x}^T K^T (diag(\hat{\xi}))^T B^T (\gamma P)x \\ + x^T (\gamma P)B(diag(\hat{\xi}))K\tilde{x} \\ + \tilde{x}^T (\dot{Q} + (A - LC)^T Q + Q(A - LC))\tilde{x} \\ + \varepsilon^T (\dot{H} + (A - LC)^T H + H(A - LC))\varepsilon \\ - \tilde{x}^T C^T G^T H\varepsilon - \varepsilon^T HGC\tilde{x} \\ - \gamma \tilde{\xi}^T (diag(u_c))^T B^T Px - \gamma x^T PB(diag(u_c))\tilde{\xi} \\ + \tilde{\xi}^T (diag(u_c))^T B^T Q\tilde{x} + \tilde{x}^T QB(diag(u_c))\tilde{\xi} \\ + \tilde{\xi}^T (diag(u_c))^T B^T H\varepsilon + \varepsilon^T HB(diag(u_c))\tilde{\xi} \\ + \tilde{\xi}^T \Gamma^{-1}\dot{\tilde{\xi}} + \dot{\tilde{\xi}}^T \Gamma^{-1}\tilde{\xi} \end{pmatrix} \tag{B.6}$$

It can be shown that [3]

$$\begin{pmatrix} -\tilde{\xi}^T (diag(u_c))^T B^T Px - x^T PB(diag(u_c))\tilde{\xi} \\ + \tilde{\xi}^T (diag(u_c))^T B^T Q\tilde{x} + \tilde{x}^T QB(diag(u_c))\tilde{\xi} \\ + \tilde{\xi}^T (diag(u_c))^T B^T H\varepsilon + \varepsilon^T HB(diag(u_c))\tilde{\xi} \end{pmatrix} \leq \begin{pmatrix} \tilde{\xi}^T (diag(u_c))^T B^T Qe_f + e_f^T QB(diag(u_c))\tilde{\xi} \\ + au_c^T u_c + \frac{1}{a} \varepsilon^T (H + Q)BB^T (H + Q)\varepsilon \\ + bu_c^T u_c + \frac{\gamma^2}{b} x^T PBB^T Px \end{pmatrix}$$

Given

$$u_c = K\hat{x} = K(x + \tilde{x}),$$

we therefore have  $au_c^T u_c = a(x + \tilde{x})^T K^T K(x + \tilde{x})$ . Thus, (B.6) becomes

$$\dot{V} \leq \begin{bmatrix} x \\ \tilde{x} \\ \varepsilon \end{bmatrix}^T \Sigma \begin{bmatrix} x \\ \tilde{x} \\ \varepsilon \end{bmatrix} + \begin{pmatrix} \tilde{\xi}^T (\text{diag}(u_c))^T B^T Q e_f \\ + e_f^T Q B (\text{diag}(u_c)) \tilde{\xi} \\ + \tilde{\xi}^T \Gamma^{-1} \dot{\xi} + \dot{\xi}^T \Gamma^{-1} \tilde{\xi} \end{pmatrix},$$

where

$$\Sigma = \begin{pmatrix} \Sigma_{11} & \Sigma_{12} \\ \Sigma_{21} & \Sigma_{22} \end{pmatrix}, \quad \Sigma_{21} = \Sigma_{12}^T$$

$$\Sigma_{11} = \gamma \begin{pmatrix} \dot{P} + (A + B(\text{diag}(\hat{\xi}))K)^T P \\ + P(A + B(\text{diag}(\hat{\xi}))K) + \bar{c}K^T K + \frac{\gamma}{b} PBB^T P \end{pmatrix}$$

$$\Sigma_{12} = \left[ \gamma (PB(\text{diag}(\hat{\xi}))K + \bar{c}K^T K) \quad 0 \right]$$

$$\Sigma_{22} = \begin{pmatrix} \begin{pmatrix} \dot{Q} + (A - LC)^T Q \\ + Q(A - LC) \\ + cK^T K \end{pmatrix} & -(HGC)^T \\ -HGC & \begin{pmatrix} \dot{H} + (A - LC)^T H \\ + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{pmatrix} \end{pmatrix}$$

and  $c = a + b$  and  $c = \gamma \bar{c}$ . Moreover, it is sufficient to require

$$\Sigma < 0 \tag{B.7}$$

and

$$\begin{pmatrix} \tilde{\xi}^T (\text{diag}(u_c))^T B^T Q e_f + e_f^T Q B (\text{diag}(u_c)) \tilde{\xi} \\ + \tilde{\xi}^T \Gamma^{-1} \dot{\xi} + \dot{\xi}^T \Gamma^{-1} \tilde{\xi} \end{pmatrix} \leq 0 \tag{B.8}$$

By applying the Schur complement [1], (B.7) can be equivalent written as

$$\Omega < 0 \tag{B.9}$$

where

$$\Omega = \begin{pmatrix} \begin{pmatrix} \dot{Q} + (A - LC)^T Q + Q(A - LC) \\ + cK^T K + \gamma F \end{pmatrix} & -C^T G^T H \\ -HGC & \begin{pmatrix} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{pmatrix} \end{pmatrix}$$

and

$$\begin{pmatrix} \dot{P} + (A + B(\text{diag}(\hat{\xi}))K)^T P \\ + P(A + B(\text{diag}(\hat{\xi}))K) \\ + \bar{c}K^T K + \frac{\gamma}{b} PBB^T P \end{pmatrix} < 0 \tag{B.10}$$

where

$$F = - \begin{pmatrix} PB(\text{diag}(\hat{\xi}))K \\ + \bar{c}K^T K \end{pmatrix} \begin{pmatrix} (A + B(\text{diag}(\hat{\xi}))K)^T P \\ + P(A + B(\text{diag}(\hat{\xi}))K) \\ + \bar{c}K^T K + \frac{\gamma}{b} PBB^T P + \dot{P} \end{pmatrix}^{-1} \begin{pmatrix} PB(\text{diag}(\hat{\xi}))K \\ + \bar{c}K^T K \end{pmatrix}$$

Note that (B.9) can be shown to be equivalent to

$$\dot{Q} + (A - LC)^T Q + Q(A - LC) + cK^T K + \gamma F < 0 \tag{B.11}$$

$$\dot{H} + (A - LC)^T H + H(A - LC) + \frac{1}{a}(H + Q)BB^T(H + Q) < 0 \tag{B.12}$$

Proof. By the Schur complement (B.9) can be equivalent written as

$$\begin{pmatrix} \begin{pmatrix} \dot{Q} + (A - LC)^T Q + Q(A - LC) \\ + cK^T K + \gamma F \end{pmatrix} \\ -C^T G^T H \begin{pmatrix} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{pmatrix}^{-1} HGC < 0 \end{pmatrix} < 0 \tag{B.13}$$

and

$$\begin{pmatrix} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{pmatrix} < 0 \tag{B.14}$$

Sufficient condition ( $\Rightarrow$ ): This direction is readily proved.

Necessary condition ( $\Leftarrow$ ): Given (B.13) and (B.14), there always exists a scalar  $\rho > 0$  and  $G = \rho \bar{G}$  such that

$$\rho^2 \alpha - \beta > 0 \tag{B.15}$$

where  $\beta = \text{eig}_{\max}[\dot{Q} + (A - LC)^T Q + Q(A - LC) + cK^T K + \gamma F]$

$$\alpha = \text{eig}_{\min} \left[ C^T \bar{G}^T H \begin{pmatrix} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{pmatrix}^{-1} H \bar{G} C \right]$$

Hence from (B.10), (B.11), and (B.12) we conclude that (B.7) is equivalent to the following three matrix inequalities:

$$\begin{pmatrix} \dot{P} + (A + B(\text{diag}(\hat{\xi}))K)^T P \\ + P(A + B(\text{diag}(\hat{\xi}))K) \\ + \bar{c}K^T K + \frac{\gamma}{b} PBB^T P \end{pmatrix} < 0 \quad (\text{B.16})$$

$$\dot{Q} + (A - LC)^T Q + Q(A - LC) + cK^T K + \gamma F < 0 \quad (\text{B.17})$$

$$\begin{pmatrix} \dot{H} + (A - LC)^T H + H(A - LC) \\ + \frac{1}{a}(H + Q)BB^T(H + Q) \end{pmatrix} < 0 \quad (\text{B.18})$$

[3] proves that (B.8) can be implied by

$$\dot{\hat{\xi}}(t) = \begin{cases} -\Gamma(\text{diag}(u_c))^T B^T Q e_f & \forall \hat{\xi}(t) \in D \\ -\Gamma W \hat{\xi}(t) - \Gamma(\text{diag}(u_c))^T B^T Q e_f & \forall \hat{\xi}(t) \in \bar{D} \end{cases} \quad (\text{B.19})$$

where

$$D = \left\{ \hat{\xi}(t) \mid \|\hat{\xi}(t)\|^2 \leq \frac{\lambda_m m}{\sigma_m} \right\}, \quad \bar{D} = \left\{ \hat{\xi}(t) \mid \|\hat{\xi}(t)\|^2 > \frac{\lambda_m m}{\sigma_m} \right\}$$

where the  $m$  is number of actuators.  $\lambda_m$  and  $-\sigma_m$  are the maximum eigenvalues of  $W^T S^{-1} W > 0$  and  $-W - W^T + S < 0$ , respectively, for some positive definite symmetric matrices  $W$  and  $S$ .

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